

Figure 4. Critical density-composition relations of binary systems of PFMCH with isomeric hexanes. Predicted values: (---). Experimental points: (•) 2,2-dimethylbutane; (O) *n*-hexane; (◊) 2-methylpentane;  $(\nabla)$  2,3-dimethylbutane; (D) 3-methylpentane.  $\xi = 0.885$  for all systems.

#### densitv ß Έ interaction coefficient

## Subscripts

1, 2 component 1, 2 С critical

- pseudocritical value for mixture cm
- component i, j 1, 1
- vap vaporization
- differentiation with respect to x, vx, v

#### Superscripts

- G gas
- liquid L

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# Study of the Critical and Azeotropic Behavior of Binary Mixtures. 2. **PVT-x** Data and Azeotropic States of Perfluoromethylcyclohexane–Isomeric Hexane Systems

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PVT-x data for five binary systems composed of the isomers of hexane with perfluoromethylcyclohexane as the common component are reported in this paper. All of these systems form positive azeotropes which persist in their critical regions. The locus of azeotropic points for each system and its prediction using an extended corresponding states principle is also reported.

## Introduction

An investigation of the PVT-x relations of a series of binary systems composed of the isomers of hexane with perfluoromethylcyclohexane (PFMCH) as a common component was undertaken to obtain information on the relative effect of molecular structure on the phase diagrams of such mixtures. These systems were found to form positive azeotropes which persist up to the critical locus curve. The critical loci of PFMCH-isomeric hexane mixtures and their correlation and prediction using an extended corresponding states principle were reported in part 1 of this paper (1). It was found that the critical loci of all these systems exhibit a minimum temperature point which is characteristic of systems which form positive azeotropes in their critical region. It was further shown that the critical loci of PFMCH-isomeric hexane systems could be predicted by the extended corresponding states approach, using only a single adjustable binary interaction coefficient obtained from the correlation of the critical states of PFMCH-n-hexane mixtures.

In this paper, we report the measurements of dew and bubble points as well as azeotropic states of PFMCH-isomeric hexane systems. The predictive capabilities of the extended corre-

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 Table I.
 Perfluoromethylcyclohexane (1)-n-Hexane (2) Data

|         | dew point   |   | bubble point |   |   |
|---------|-------------|---|--------------|---|---|
| temp, K | press., bar | vol, cm <sup>3</sup><br>mol <sup>-1</sup> | press., bar  | vol, cm <sup>3</sup><br>mol <sup>-1</sup> |   |
|         |             | $x_{1} = 0.8171$                          |              |   | - |
| 478 16  | 21 364      | 620.26                                    | 21 554       | 100 65                                    |   |
| 474 11  | 10 6 20     | 020.20                                    | 21.334       | 499.03                                    |   |
| 4/4.11  | 19.620      | 908.21                                    | 20.507       | 3/6.01                                    |   |
| 468.12  | 17.693      | 1137.41                                   | 18.774       | 337.41                                    |   |
| 463.04  | 16.145      | 1339.56                                   | 17.384       | 317.64                                    |   |
| 453.13  | 13.540      | 1755.18                                   | 14.823       | 295.80                                    |   |
| 443.02  | 11.240      | 2239.46                                   | 12.543       | 280.52                                    |   |
| 433.08  | 9.201       | 2849.55                                   | 10.577       | 266.65                                    |   |
| 423.00  | 7.587       | 3605.39                                   | 8.881        | 257.08                                    |   |
| 403.07  | 4.912       | 5727.12                                   | 6.154        | 240.47                                    |   |
| 383.07  | 3.092       | 9232.89                                   | 4.126        | 228.27                                    |   |
|         |             | x = 0.6602                                |              |   |   |
| 472 67  | 01 071      | $x_1 = 0.0003$                            | 22.1.40      | 126.61                                    |   |
| 4/3.0/  | 21.9/1      | 605.06                                    | 22.148       | 436.61                                    |   |
| 469.12  | 20.178      | 866.66                                    | 20.690       | 351.94                                    |   |
| 464.10  | 18.510      | 1051.94                                   | 19.163       | 321.57                                    |   |
| 453.07  | 15.256      | 1471.77                                   | 16.050       | 289.17                                    |   |
| 443.02  | 12.764      | 1889.74                                   | 13.619       | 275.51                                    |   |
| 423.00  | 8.751       | 2979.20                                   | 9.560        | 250.00                                    |   |
| 403.12  | 5.688       | 4841.68                                   | 6.459        | 231.31                                    |   |
| 383.07  | 3.432       | 8141.80                                   | 4.257        | 212.33                                    |   |
|         |             | r = 0.4860                                |              |   |   |
| 473 51  | 23 288      | x1 - 0.4000                               | 22 210       | 502 70                                    |   |
| 460 10  | 23.200      | 795 40                                    | 23.310       | 302.79                                    |   |
| 462.05  | 10 6 21     | /03.42                                    | 21.745       | 330.03                                    |   |
| 403.03  | 19.031      | 980.33                                    | 19.700       | 303.60                                    |   |
| 433.09  | 10.550      | 1320.07                                   | 16.//8       | 276.23                                    |   |
| 443.02  | 13.862      | 1681.91                                   | 14.119       | 254.61                                    |   |
| 422.99  | 9.588       | 2641.88                                   | 9.875        | 233.79                                    |   |
| 403.07  | 6.318       | 4330.21                                   | 6.700        | 216.44                                    |   |
| 383.02  | 4.128       | 6804.37                                   | 4.347        | 210.46                                    |   |
|         |             | $x_1 = 0.3342$                            |              |   |   |
| 478.25  | 24,769      | 525.35                                    | 24,873       | 417.15                                    |   |
| 473.10  | 22.741      | 760.95                                    | 22 946       | 308.65                                    |   |
| 468.10  | 20.956      | 918.54                                    | 21 1 70      | 285 22                                    |   |
| 463.04  | 19.327      | 1069 16                                   | 19 54 5      | 269.76                                    |   |
| 453.09  | 16 401      | 1388 47                                   | 16 694       | 248 20                                    |   |
| 443.02  | 13 780      | 1758 57                                   | 14 027       | 240.20                                    |   |
| 472.02  | 9 5 9 7     | 2711 47                                   | 0 937        | 216.60                                    |   |
| 403 13  | 6 41 9      | A100 17                                   | 5.637        | 210.00                                    |   |
| 202.00  | 4 1 2 2     | 4133.17                                   | 4 2 2 1      | 203.00                                    |   |
| 363.03  | 4.125       | 0455.01                                   | 4.551        | 189.19                                    |   |
|         |             | $x_1 = 0.1731$                            |              |   |   |
| 489.75  | 27.258      | 529.35                                    | 27.517       | 382.30                                    |   |
| 484.12  | 24.833      | 742.92                                    | 25.518       | 289.24                                    |   |
| 478.11  | 22.540      | 915.14                                    | 23.417       | 264.54                                    |   |
| 473.10  | 20.795      | 1055.22                                   | 21.745       | 253.06                                    |   |
| 463.04  | 17.621      | 1351.93                                   | 18.651       | 232.88                                    |   |
| 452.99  | 14.931      | 1693.39                                   | 15.888       | 219.85                                    |   |
| 443.03  | 12.556      | 2086.00                                   | 13.497       | 212.29                                    |   |
| 423.00  | 8 675       | 2952.99                                   | 9475         | 195.01                                    |   |
| 403.07  | 5 600       | 5064.97                                   | 6 4 5 6      | 182.24                                    |   |
| 383 19  | 3 547       | 7949 79                                   | 4 255        | 174 56                                    |   |
| 505.12  | 5.547       | ,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,   | 4.233        | 174.50                                    |   |
|         |             | $x_1 = 0.000$                             |              |   |   |
| 507.50  | 30.336      | 423.84                                    | 30.268       | 330.29                                    |   |
| 503.21  | 28.478      | 627.46                                    | 28.564       | 281.14                                    |   |
| 493.11  | 24.501      | 880.92                                    | 24.619       | 241.74                                    |   |
| 483.11  | 21.159      | 1116.86                                   | 21.209       | 223.58                                    |   |
| 473.10  | 18.084      | 1410.35                                   | 18.256       | 210.15                                    |   |
| 463.04  | 15.348      | 1712.72                                   | 15.468       | 199.35                                    |   |
| 453.08  | 12.890      | 2106.99                                   | 13.030       | 190.50                                    |   |
| 443.02  | 10.833      | 2544.73                                   | 10.951       | 182.22                                    |   |
| 422.99  | 7.437       | 3849.80                                   | 7.544        | 170.73                                    |   |
| 403.07  | 4.963       | 5643.05                                   | 4.969        | 162.60                                    |   |
| 383.19  | 3.137       | 7867.47                                   | 3.161        | 155.87                                    |   |

sponding states method are tested further, and the method is used for the calculation of azeotropic loci of binary systems of PFMCH with the isomeric hexanes.

#### **Experimental Section**

The experimental details have been reported fully in part 1 and are not repeated here.



Figure 1. Pressure-temperature phase diagram for the PFMCH-*n*-hexane system: (**(()**) critical points of mixtures.



Figure 2. Pressure-composition diagram for the PFMCH-*n*-hexane system: (---) locus of azeotropes; ( $\phi$ ) calculated critical locus curve of system.

# Results

Results in the Vapor-Liquid Region for the Binary System. The pressure, temperature, and specific volume data for the vapor-liquid region for the five binary systems are presented in Tables I–V. The data cover a range from 383.16 K and a pressure of approximately  $\sim$ 3.45 bar to the highest temperature and pressure at which liquid and vapor coexist. Only selected data points are presented in Tables I–V. Detailed results can be found in ref 2.

Rather than present several repetitious  $PVT-x_1$  diagrams for each of the five binary systems, we chose the perfluoromethylcyclohexane-*n*-hexane system as a representative sample, and data from Table I were employed to construct *PT*,  $P-x_1$  and *TV* diagrams; these diagrams are presented as Figures 1, 2, and 3, respectively.

**Azeotropic States.** At a given temperature, the azeotropic pressure and composition were determined by using the Gibbs-Konowalow theorem. The theorem states (4), "If in a series of isothermal equilibrium states of a two phase binary system, the composition of the two phases becomes the same, then the pressure must pass through an extreme value." Thus,

Table II. Perfluoromethylcyclohexane-3-Methylpentane Data

|         | dew point      |                      | bubble point |                      |
|---------|----------------|----------------------|--------------|----------------------|
|         | <del></del>    | vol. cm <sup>3</sup> | - <u></u>    | vol. cm <sup>3</sup> |
| temp, K | press., bar    | moΓ¹                 | press., bar  | mol <sup>-1</sup>    |
|         |                | x = 0.7951           |              |                      |
| 476.66  | 21.319         | 685.16               | 21.734       | 427.60               |
| 473.10  | 19.903         | 879.89               | 20.708       | 368.09               |
| 463.04  | 16.618         | 1271.67              | 17.827       | 317.40               |
| 453.09  | 13.869         | 1676.19              | 15.112       | 291.98               |
| 443.02  | 11.461         | 2160.88              | 12.837       | 275.54               |
| 422.99  | 7.641          | 3561.71              | 9.060        | 251.70               |
| 403.07  | 4.988          | 5572.22              | 6.191        | 236.31               |
| 383.06  | 3.141          | 8841.47              | 4.118        | 223.97               |
|         |                | $x_1 = 0.5869$       |              |                      |
| 472.67  | 22.996         | 564.78               | 23.166       | 428.72               |
| 468.10  | 21.130         | 803.44               | 21.569       | 337.92               |
| 463.04  | 19.372         | 1006.21              | 20.101       | 310.47               |
| 453.09  | 16.299         | 1346.46              | 17.086       | 281.74               |
| 443.02  | 13.600         | 1745.58              | 14.453       | 262.72               |
| 422.99  | 9.116          | 2899.56              | 10.199       | 238.39               |
| 403.07  | 6.136          | 4477.32              | 7.013        | 222.96               |
| 383.06  | 3.858          | 7164.52              | 4.687        | 209.53               |
|         |                | $x_1 = 0.4045$       |              |                      |
| 474.06  | 24.502         | 559.29               | 24.641       | 370.73               |
| 468.10  | 22.192         | 804.52               | 22.513       | 301.97               |
| 462.57  | 20.239         | 979.25               | 20.657       | 279.90               |
| 453.09  | 17.327         | 1269.48              | 17.724       | 257.93               |
| 443.02  | 14.611         | 1615.28              | 15.053       | 241.47               |
| 423.00  | 10.149         | 2516.07              | 10.633       | 220.23               |
| 403.07  | 6.846          | 3950.64              | 7.314        | 205.96               |
| 383.06  | 4.435          | 6151.45              | 4.918        | 190.61               |
|         |                | $x_1 = 0.2952$       |              |                      |
| 478.44  | 25.709         | 520.32               | 25.833       | 365.10               |
| 474.10  | 23.946         | 710.03               | 24.261       | 300.99               |
| 468.10  | 21.754         | 889.19               | 22.132       | 271.47               |
| 463.04  | 20.121         | 1026.81              | 20.529       | 257.29               |
| 453.09  | 17.057         | 1325.52              | 17.462       | 238.60               |
| 443.02  | 14.405         | 1662.30              | 14.791       | 225.36               |
| 422.99  | 10.021         | 2594.03              | 10.419       | 207.00               |
| 403.07  | 6.792          | 3934.01              | 7.165        | 192.98               |
| 383.06  | 4.404          | 6185.02              | 4.722        | 182.12               |
|         |                | $x_1 = 0.2062$       |              |                      |
| 484.11  | 27.132         | 529.08               | 27.411       | 358.26               |
| 478.10  | 24.592         | 753.10               | 25.210       | 283.15               |
| 473.14  | 22.704         | 889.07               | 23.441       | 262.10               |
| 463.04  | 19.297         | 1173.52              | 20.140       | 239.29               |
| 453.09  | 16.374         | 1470.90              | 17.172       | 224.38               |
| 443.07  | 13.794         | 1833.90              | 14.584       | 213.68               |
| 403.07  | 5.002<br>6.474 | 2021.34<br>A13A 21   | 7 1 1 1      | 193.33               |
| 383.06  | 4 163          | 6453 76              | 4 698        | 172 37               |
| 505.00  | 4.105          | 0433.70              | 4.070        | 1/2.5/               |
| 494 01  | 29 252         | $x_1 = 0.0855$       | 20 400       | 310 56               |
| 489 11  | 26 790         | 687 31               | 27.407       | 267 20               |
| 483.11  | 24,399         | 844 21               | 25.089       | 245.97               |
| 473.10  | 20.932         | 1087.75              | 21.685       | 224.91               |
| 463.04  | 17.808         | 1371.02              | 18.635       | 211.19               |
| 443.02  | 12.777         | 2066.43              | 13.513       | 192.73               |
| 422.93  | 8.887          | 3148.33              | 9.589        | 181.42               |
| 403.07  | 5.998          | 4592.39              | 6.545        | 171.13               |
| 383.06  | 3.792          | 7466.38              | 4.357        | 162.33               |

if the bubble and dew point pressures are plotted against composition at a given temperature and smooth curves are drawn through the data, both curves will exhibit a maximum, for positive azeotropy, at the azeotropic composition.

The method was applied to each system at temperatures from 398.16 K to the critical region by using increments of 5 K. When smooth values of the bubble and dew point data were plotted, as indicated above, two well-defined curves were obtained. For each temperature, the maxima on these curves could reliably be established. It was also observed that both maxima occurred at approximately the same composition. An average of the two values was taken as the experimental azeotropic pressure and



Figure 3. Temperature-volume diagram for PFMCH-n-hexane system.



**Figure 4.** Composite log  $P^A$  vs. log  $x_1^A$  diagram of the PFMCH-isomeric hexane systems: (---) critical locus curve; (O)*n*-hexane; ( $\Box$ ) 3-methylpentane; ( $\diamond$ ) 2-methylpentane; ( $\nabla$ ) 2,3-dimethylbutane; ( $\bullet$ ) 2,2-dimethylbutane.

composition. The results of these equations are presented in Table VI.

#### **Correlation of the Data**

**Pressure – Temperature Correlation.** A correlation described by Prigogine (4) was applied to the data in Table VI. Prigogine showed that the azeotropic pressure ( $P^A$ ) can be related to the temperature (T) by the standard vapor pressure equation

$$\log \left(P^{A}\right) = A + B/T \tag{1}$$

where  $P^A$  is in bars, T is in K, and A and B are constants. Equation 1 shows that the log of the azeotropic pressure is linear in 1/T. The constants A and B were determined by a leastsquares fit to the data and are presented in Table VII.

**Pressure** – **Composition Correlation.** The relationship between the azeotropic composition and the pressure is expressed satisfactorily by the equation of Othmer and Ten Eyck (3)

$$\log (P^{A}) = a + b(\log x_{1}^{A})$$
(2)

where  $x_1$  is the mole fraction of PFMCH and  $P^A$  the azeotropic pressure. The least-squares constants *a* and *b* for each system are listed in Table VIII.

The azeotropic composition  $x_1$  changes very little with pressure. This results from the fact that the temperature coefficients of the vapor pressure (dP/dT) for PFMCH and the hexanes are approximately the same. It is only when these coefficients are quite different from each other that the composition changes rapidly with the pressure.

 Table III.
 Perfluoromethylcyclohexane-2-Methylpentane Data

Table IV. Perfluoromethylcyclohexane (1)-2,3-Dimethylbutane (2) Data

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|         | dew p                 | ooint                | bu <b>b</b> ble point |                      |
|---------|-----------------------|----------------------|-----------------------|----------------------|
|         |                       | vol. cm <sup>3</sup> |                       | vol. cm <sup>3</sup> |
| temp, K | press., bar           | mol <sup>-1</sup>    | press., bar           | mol <sup>-1</sup>    |
|         |                       | 0.0000               |                       |                      |
| 475 10  | 20.952                | $c_1 = 0.7980$       | 01.460                | 412.45               |
| 4/5.10  | 20.853                | /33.88               | 21.463                | 413.45               |
| 468.10  | 18.286                | 1072.04              | 19.372                | 344.43               |
| 463.04  | 16./00                | 12/5.39              | 17.950                | 322.92               |
| 453.09  | 13.855                | 1699.48              | 15.341                | 293.43               |
| 443.02  | 11.394                | 2212.02              | 13.048                | 277.07               |
| 423.00  | 7.632                 | 3609.93              | 9.192                 | 252.90               |
| 403.11  | 5.039                 | 5596.76              | 6.331                 | 237.09               |
| 383.06  | 3.107                 | 9063.53              | 4.204                 | 223.82               |
|         | x                     | $z_1 = 0.6087$       |                       |                      |
| 471.07  | 22.597                | 577.14               | 22.734                | 457.43               |
| 468.10  | 21.315                | 777 <b>.89</b>       | 21.786                | 361.95               |
| 463.04  | 19.495                | 980.57               | 20.143                | 325.39               |
| 453.09  | 16.382                | 1339.65              | 17.206                | 291.34               |
| 443.02  | 13.581                | 1764.92              | 14.573                | 271.07               |
| 422.99  | 9.105                 | 2918.49              | 10.297                | 243.49               |
| 403.07  | 6.105                 | 4548.69              | 7.023                 | 227.20               |
| 383.06  | 3.773                 | 7477.78              | 4.615                 | 210.45               |
|         |                       | - 0 4104             |                       |                      |
| 470 78  | 24 094                | 527 71               | 24 238                | 296.91               |
| 463.04  | 21.034                | 862 50               | 24.230                | 208 11               |
| 452.00  | 17 900                | 1171 40              | 19 494                | 290,11               |
| 433.09  | 15.046                | 1520 49              | 16,404                | 200.33               |
| 422.00  | 10.270                | 1320.40              | 11 166                | 247.30               |
| 402.07  | 6 01 9                | 2373.27              | 7 701                 | 222,37               |
| 403.07  | 0.910                 | 5650.50              | 5 1 6 7               | 200.89               |
| 362.98  | 4.400                 | 0001.19              | 5.10/                 | 192.28               |
|         | x                     | $x_1 = 0.3077$       |                       |                      |
| 473.73  | 25.076                | 532.55               | 25.208                | 374.58               |
| 469.10  | 23.237                | 739.44               | 23.519                | 305.35               |
| 463.04  | 21.055                | 923.11               | 21,419                | 276.47               |
| 453.09  | 17.882                | 1218.06              | 18.280                | 252.61               |
| 442.98  | 15.061                | 1550.50              | 15.513                | 236.62               |
| 423.00  | 10.499                | 2341.76              | 10.968                | 213.36               |
| 403.07  | 7.110                 | 3776.26              | 7.511                 | 199.81               |
| 383.06  | 4.535                 | 5976.62              | 4.970                 | 186.68               |
|         | Y                     | = 0.2059             |                       |                      |
| 478.67  | 26.243                | 547.67               | 26.392                | 357.79               |
| 474.10  | 24,310                | 720.73               | 24.670                | 291.92               |
| 468.10  | 22.099                | 882.65               | 22.500                | 264.99               |
| 463.04  | 20.346                | 1022.87              | 20 803                | 251 61               |
| 453.09  | 17 310                | 1316.63              | 17 744                | 233 41               |
| 443 02  | 14.600                | 1649 94              | 15.051                | 220.01               |
| 423.00  | 10142                 | 2554 82              | 10 636                | 200.88               |
| 403.00  | 6 8 2 8               | 2007.02              | 7 749                 | 186 49               |
| 383 04  | 0.030<br><u>1</u> 210 | 6748 70              | 1.200                 | 175 22               |
| 565.00  | 7.310                 | 0270.27              | 7.755                 | 113.23               |
| 405.11  | x                     | 1 = 0.0913           |                       |                      |
| 487.41  | 28.324                | 490.10               | 28.578                | 345.59               |
| 484.11  | 26.795                | 630.98               | 27.352                | 287.35               |
| 473.05  | 22.494                | 926.94               | 23.322                | 241.32               |
| 463.04  | 19.160                | 1192.63              | 20.075                | 223.49               |
| 443.02  | 13.684                | 1854.66              | 14.645                | 200.96               |
| 423.00  | 9.531                 | 2854.78              | 10.446                | 185.65               |
| 403.07  | 6.411                 | 4227.32              | 7.230                 | 174.44               |
| 383.06  | 4.122                 | 6447.19              | 4.819                 | 163.16               |
|         |                       |                      |                       |                      |

**Estimation of the Critical Azeotropes.** Figure 4 is a plot of log  $P^A$  vs. log  $(x_1^A)$  for the PFMCH-*n*-hexane system and serves to illustrate the method that was employed to estimate the critical azeotropes. The data in Figure 4 fall very close to a straight line from the lowest to the highest pressures. By the extension of this straight line to the critical locus curve, the critical azeotrope for the system can be approximated. The quantities marked with an asterisk in Table VI represent the critical azeotropes obtained in this manner.

The critical azeotrope must not be confused with the minimum temperature point in the  $T_c$  vs.  $x_1$  curve. Thus, in the PFMCH-*n*-hexane system, the critical azeotrope is seen to occur at a mole fraction of 0.464 and not at the minimum critical temperature, where  $x_1 = 0.550$ .

|         | dew point   |                      | bubble point |                      |
|---------|-------------|----------------------|--------------|----------------------|
|         |             |                      |              | <u> </u>             |
|         |             | vol, cm <sup>3</sup> |              | vol, cm <sup>3</sup> |
| temp, K | press., bar |                      | press., oar  | moi -                |
|         |             | $x_1 = 0.8173$       |              |                      |
| 477.87  | 21.547      | . 633.61             | 21.836       | 490.77               |
| 473.10  | 19.570      | 920.74               | 20.563       | 364.86               |
| 463.04  | 16.201      | 1353.59              | 17.727       | 317.19               |
| 453.09  | 13.695      | 1704.46              | 15.164       | 290.46               |
| 443.02  | 11.294      | 2193.61              | 12,930       | 272.95               |
| 423.00  | 7 600       | 3570.24              | 9 1 8 5      | 250.50               |
| 403 11  | 4 952       | 5658.05              | 6 3 5 9      | 235.05               |
| 39310   | 3 0 5 9     | 013212               | 3 5 80       | 233.03               |
| 303.10  | 5.059       | 91 52.12             | 2200         | 222.07               |
|         |             | $x_1 = 0.5930$       |              |                      |
| 472.11  | 23.118      | 553.57               | 23.237       | 425.32               |
| 468.10  | 21.260      | 786.47               | 21.989       | 337.73               |
| 463.04  | 19.443      | 972.28               | 20.389       | 308.13               |
| 453.09  | 16.347      | 1314.48              | 17.486       | 277.66               |
| 443.02  | 13.669      | 1697.57              | 14.899       | 268.27               |
| 423.00  | 9.185       | 2798.61              | 10.629       | 235.69               |
| 403.07  | 5.998       | 4496.77              | 7.379        | 220.03               |
| 383.07  | 3.802       | 7172.72              | 4.976        | 207.70               |
|         |             | 0.441.7              |              |                      |
| 451 50  |             | $x_1 = 0.441/$       |              |                      |
| 471.72  | 24.210      | 512.22               | 24.289       | 398.93               |
| 468.1   | 22.735      | 715.98               | 23.002       | 319.78               |
| 463.04  | 20.873      | 887.73               | 21.259       | 291.56               |
| 453.09  | 17.695      | 1190.17              | 18.103       | 264.63               |
| 443.02  | 14.913      | 1532.68              | 15.393       | 245.51               |
| 423.00  | 10.975      | 2410.94              | 10.870       | 222.30               |
| 403.07  | 6.946       | 3796.65              | 7.446        | 208.79               |
| 383.06  | 4.331       | 6241.12              | 4.941        | 197.40               |
|         |             | r = 0.2875           |              |                      |
| 475 78  | 25 943      | 483.47               | 26.069       | 335.82               |
| 473.10  | 23.943      | 612.22               | 25.081       | 295.02               |
| 463.04  | 24.009      | 887 37               | 21 530       | 295.05               |
| 453.04  | 18 028      | 1152 21              | 18 406       | 272.77               |
| 443.01  | 15 224      | 1465 04              | 15 665       | 223.72               |
| 422.00  | 10 702      | 2244 57              | 11 101       | 109 40               |
| 402.07  | 7 252       | 2472 69              | 7 605        | 194 27               |
| 392.06  | 1.233       | 5364.06              | 5 1 24       | 176 27               |
| 363.00  | 4./40       | 3304.90              | 5.124        | 1/0.2/               |
|         |             | $x_1 = 0.2030$       |              |                      |
| 481.31  | 27.498      | <b>490.00</b>        | 27.629       | 356.15               |
| 478.10  | 26.091      | 632.69               | 26.457       | 296.18               |
| 473.10  | 24,065      | 785.50               | 24.564       | 269.05               |
| 463.04  | 20.588      | 1039.52              | 21.136       | 243.53               |
| 453.09  | 17.553      | 1314.37              | 18,112       | 225.38               |
| 443.02  | 14.858      | 1643.96              | 15.402       | 213.41               |
| 423.00  | 10.454      | 2434.98              | 10.973       | 196.29               |
| 403.07  | 7 1 2 7     | 3793 68              | 7 578        | 184 38               |
| 383.09  | 4 6 3 9     | 587915               | 5 050        | 73.88                |
| 000107  |             |                      | 0.000        | / 0100               |
| 400 55  | 00.041      | $x_1 = 0.1078$       | 00 505       | 001.00               |
| 488.77  | 29.361      | 468.41               | 29.597       | 331.80               |
| 484.11  | 27.230      | 641.62               | 27.830       | 271.16               |
| 474.14  | 23.317      | 891.97               | 24.099       | 236.48               |
| 463.05  | 19.678      | 1175.26              | 20.564       | 217.53               |
| 453.07  | 16.748      | 1449.75              | 17.546       | 205.84               |
| 443.02  | 14.140      | 1790.57              | 15.051       | 196.50               |
| 423.00  | 9.936       | 2732.23              | 10.747       | 182.34               |
| 403.07  | 6.724       | 4061.59              | 7.472        | 171.11               |
| 383.06  | 4.388       | 6215.12              | 5.034        | 161.80               |

#### **Prediction of Azeotropic Loci**

A binary azeotrope is a state in which the pressure, temperature, chemical potentials (or fugacities) of the components, and composition are the same in both liquid and gas. At a given temperature, it is defined by eq 3–5, where the superscripts refer

$$P^{\rm G} = P^{\rm L} \tag{3}$$

$$f_1^{\mathbf{G}} = f_1^{\mathbf{L}} \tag{4}$$

$$f_2^{\mathbf{G}} = f_2^{\mathbf{G}} \tag{5}$$

to the vapor and liquid phases. At any temperature, these three

Table V. Perfluoromethylcyclohexane-2,2-Dimethylbutane Data



**Figure 5.** Comparison of experimental and predicted *PT* and *T*-*x* relations along the azeotropic loci of binary systems of PFMCH with the isomeric hexanes ( $\xi_{12} = 0.885$ ). Predicted: (---). Experimental data points:

| hydrocarbon + PFMCH            | PT<br>chart | <i>T-x</i> chart |
|--------------------------------|-------------|------------------|
| (0) <i>n</i> -hexane           | Α           | В                |
| (a) 2,3-dimethylbutane         | Α           | В                |
| ( $\diamond$ ) 2-methylpentane | С           | D                |
| (•) 2,2-dimethylbutane         | С           | D                |
| (a) 3-methylpentane            | E           | F                |

equations may be solved for the three unknowns  $V^{G}$ ,  $V^{L}$ , and x, provided expressions are available for the pressure and for the fugacity of each component in the mixture.

In the calculations presented below, the equations for the pressure and for the fugacities were obtained by using the extended form of the corresponding states principle with methane as the reference fluid. The extension of the principle to PFMCH and the hexane isomers required only the critical properties and acentric factors of the pure substances as input parameters. The extension to mixtures was achieved via the van der Waals one-fluid model:

$$\mathcal{T}_{\rm cm} \mathcal{V}_{\rm cm} = \sum_{i} \sum_{I} x_i x_j \mathcal{T}_{\rm cij} \mathcal{V}_{\rm cij} \tag{6}$$

$$V_{\rm cm} = \sum_{i} \sum_{j} x_i x_j V_{\rm cij} \tag{7}$$

and the mixing rules

$$T_{\rm cm} = \xi_{\parallel} (T_{\rm c\parallel} T_{\rm c\parallel})^{1/2} \tag{8}$$

$$V_{\rm op} = (V_{\rm off}^{1/3} + V_{\rm off}^{1/3})^3 / 8 \tag{9}$$

where the binary interaction coefficient  $\xi_{ij}$  is an adjustable constant which must be obtained from experimental data on the mixture. It has been shown earlier (5) that values of  $\xi_{\mu}$  calculated from correlations of critical and azeotropic states and saturated liquid densities (6) agree very well with each other, at least for mixtures of the lower molecular weight n-alkanes and  $CO_2$ . It is convincingly demonstrated here that this is also true for PFMCH-isomeric hexane mixtures. The single value of  $\xi_{\mu} = 0.885$  used in *all* calculations presented below was obtained from a correlation of the critical states of the PFMCH-n-hexane system. Therefore, there were no adjustable constants used in the calculations reported here. The predicted azeotropic loci shown in Figure 5 were obtained solely from a knowledge of the critical properties and acentric factors of the pure components and the critical locus curve of PFMCH-nhexane mixtures. It is seen that agreement between predicted and experimental values is very good. This agreement could be improved further if the critical locus curve of each binary

|   |                 | dew point             |                     | bubble point |                     |  |  |  |
|---|-----------------|-----------------------|---------------------|--------------|---------------------|--|--|--|
|   |                 | ·                     | vol cm <sup>3</sup> |              | vol cm <sup>3</sup> |  |  |  |
|   | temp K          | ntess har             | $mol^{-1}$          | nress har    | $mol^{-1}$          |  |  |  |
| _ | temp, K         | press., bai           |                     | press., 0ai  |                     |  |  |  |
|   | $x_1 = 0.8330$  |                       |                     |              |                     |  |  |  |
|   | 477 <b>.</b> 46 | 21.334                | 662.67              | 21.703       | 476.93              |  |  |  |
|   | 471.10          | 19 <b>.</b> 909       | 875.87              | 20.821       | 380.36              |  |  |  |
|   | 463.04          | 16.316                | 1323.70             | 17.698       | 320.71              |  |  |  |
|   | 453.09          | 13.511                | 1758.54             | 15,139       | 295.14              |  |  |  |
|   | 443.02          | 10.805                | 2387.43             | 12.872       | 278.76              |  |  |  |
|   | 423.00          | 7.473                 | 3678.51             | 9.107        | 255.52              |  |  |  |
|   | 403.07          | 4.832                 | 5818.68             | 6.245        | 239.75              |  |  |  |
|   | 383.04          | 2.928                 | 9564.68             | 4,174        | 227.97              |  |  |  |
|   |                 |                       | 0 6525              |              |                     |  |  |  |
|   | 470.10          | 12 726                | $t_1 = 0.0323$      | 22.057       | 424 10              |  |  |  |
|   | 4/0.10          | 10 962                | 333.20              | 23.037       | 424.10              |  |  |  |
|   | 403.04          | 19.002                | 927.00              | 20.079       | 204 42              |  |  |  |
|   | 455.09          | 10.014                | 12/8.10             | 17.047       | 204.42              |  |  |  |
|   | 443.02          | 13.755                | 1081.04             | 15.221       | 203.72              |  |  |  |
|   | 423.00          | 9.001                 | 2899.60             | 10.844       | 239.05              |  |  |  |
|   | 403.07          | 6.003                 | 4469.29             | 7.542        | 224,10              |  |  |  |
|   | 383.10          | 3.686                 | 7349.44             | 4.989        | 212.32              |  |  |  |
|   |                 | ,                     | $x_1 = 0.4024$      |              |                     |  |  |  |
|   | 467.51          | 24.483                | 550.05              | 24.676       | 378.50              |  |  |  |
|   | 463.02          | 22.667                | 751.04              | 23.164       | 313.26              |  |  |  |
|   | 453.09          | 19.209                | 1058.71             | 19.810       | 271.74              |  |  |  |
|   | 443.02          | 16.197                | 1383.29             | 16.936       | 251.22              |  |  |  |
|   | 423.00          | 11.148                | 2246.97             | 12.118       | 226.02              |  |  |  |
|   | 403.07          | 7.382                 | 3625.92             | 8.427        | 209.16              |  |  |  |
|   | 383.07          | 4.948                 | 1440.20             | 5 736        | 197.79              |  |  |  |
|   |                 |                       | 0.0040              | 0            |                     |  |  |  |
|   | 100.00          | <b>x</b> <sub>1</sub> | = 0.2943            | 05 01 0      | 202.46              |  |  |  |
|   | 469.63          | 25.786                | 471.14              | 25,813       | 383.46              |  |  |  |
|   | 463.06          | 23.175                | 746.24              | 23.451       | 283.83              |  |  |  |
|   | 453.06          | 19.701                | 1024.75             | 20.058       | 252,14              |  |  |  |
|   | 443.02          | 16.752                | 1310.86             | 17.118       | 234.46              |  |  |  |
|   | 423.00          | 11.793                | 2060.53             | 12.342       | 212.86              |  |  |  |
|   | 403.07          | 8.061                 | 3204.06             | 8.561        | 197.70              |  |  |  |
|   | 383.09          | 5.309                 | 4953.15             | 5.782        | 186.53              |  |  |  |
|   |                 | :                     | $x_{.} = 0.2056$    |              |                     |  |  |  |
|   | 473.10          | 27.018                | 491.50              | 27.138       | 365.25              |  |  |  |
|   | 468.10          | 24.942                | 686.67              | 25.315       | 285.82              |  |  |  |
|   | 463.04          | 23.095                | 822.21              | 23.551       | 266.03              |  |  |  |
|   | 453.09          | 19.698                | 1086 10             | 20 233       | 239 16              |  |  |  |
|   | 443.02          | 16.707                | 1382.52             | 17.284       | 222.92              |  |  |  |
|   | 422.99          | 11 721                | 2144 62             | 12 375       | 204 60              |  |  |  |
|   | 403.07          | 8 1 5 2               | 3273.07             | 8 708        | 189.83              |  |  |  |
|   | 382.24          | 5 346                 | 4971 73             | 5 816        | 176 10              |  |  |  |
|   | 002.21          | 0.510                 | 10/11/10            | 0.010        | 1/0.10              |  |  |  |
|   | 401.05          |                       | $x_1 = 0.0848$      |              |                     |  |  |  |
|   | 481.05          | 28.926                | 501.73              | 29.080       | 321.84              |  |  |  |
|   | 478.10          | 27.607                | 603.28              | 27.885       | 283.21              |  |  |  |
|   | 473.1           | 25.690                | 734.85              | 25.993       | 256.49              |  |  |  |
|   | 463.06          | 22.035                | 990.06              | 22.367       | 230.53              |  |  |  |
|   | 453.11          | 18.779                | 1230.89             | 19.240       | 215.32              |  |  |  |
|   | 443.02          | 15.917                | 1550.74             | 16.443       | 205.17              |  |  |  |
|   | 422.99          | 11.246                | 2357.04             | 11.749       | 189.14              |  |  |  |
|   |                 |                       |                     |              |                     |  |  |  |

mixture were correlated individually, or if all critical and azeotropic states were correlated simultaneously. It is not the purpose of this study to obtain an "optimum" value of the binary interaction coefficient  $\xi_{ij}$ . The calculations were carried out to test the corresponding states approach on the PFMCH–isomeric hexane systems and to look at its predictive capabilities. It is obvious that both of these objectives have been met. It has been shown further that the binary interaction coefficient  $\xi_{ij}$  is a property of the forces between molecules in a mixture and its value calculated from one property can be used to predict another (related) property. Further details of the method for the calculation of azeotropic states and of the corresponding states method are given elsewhere (6, 7).

# Glossary

| Α, | В | constants |
|----|---|-----------|
| я  | h | constants |

a, b constant f fugacity

| Table VI. | Azeotropic PT-x | A Dataa |
|-----------|-----------------|---------|
|-----------|-----------------|---------|

| Т, К           | P, bar            | x <sub>1</sub> <sup>A</sup> | Т, К              | P, bar           | x <sub>i</sub> A |
|----------------|-------------------|-----------------------------|-------------------|------------------|------------------|
| Perfluorom     | ethylcyclohexane- | n-Hexane                    | Perfluoromethy    | lcyclohexane-2-M | ethylpentane     |
| 398.16         | 5.954             | 0.405                       | 433.16            | 13.032           | 0.377            |
| 403.16         | 6.612             | 0.415                       | 438.16            | 14.202           | 0.379            |
| 408.16         | 7.318             | 0.411                       | 443.16            | 15.449           | 0.381            |
| 413.16         | 8.101             | 0.416                       | 448.16            | 16.793           | 0.384            |
| 418.16         | 8.878             | 0.419                       | 453.16            | 18.246           | 0.386            |
| 423.16         | 9.828             | 0.427                       | 458.16            | 19.828           | 0.389            |
| 428.16         | 10.810            | 0.428                       | 463.16            | 21.450           | 0.390            |
| 433.16         | 11.798            | 0.433                       | 468.16            | 23.199           | 0.395            |
| 438.16         | 12.897            | 0.436                       | 471.36*           | 24.339*          | 0.399*           |
| 443.16         | 14.084            | 0.440                       |                   |                  |                  |
| 448.16         | 15.467            | 0.446                       | Periluoromethylc  | cionexane-2,3-D  |                  |
| 453.16         | 16.752            | 0.448                       | 398.16            | 0.780            | 0.289            |
| 458.16         | 18.255            | 0.451                       | 403.16            | /.488            | 0.293            |
| 463.16         | 19.771            | 0.455                       | 408.16            | 8.272            | 0.300            |
| 468.16         | 21.408            | 0.457                       | 413.16            | 9.116            | 0.301            |
| 473.16         | 23,232            | 0.463                       | 418.16            | 9.993            | 0.304            |
| 473.46*        | 23.273*           | 0.464*                      | 423.16            | 10.936           | 0.308            |
|                | 20.270            |                             | 428.16            | 11.980           | 0.310            |
| Perfluoromethy | lcyclohexane-3-M  | ethylpentane                | 433.16            | 13,101           | 0.318            |
| 398.16         | 6.422             | 0.384                       | 438.16            | 14.267           | 0.320            |
| 403.16         | 7.106             | 0.386                       | 443.16            | 15.504           | 0.325            |
| 408.16         | 7.859             | 0.387                       | 448.16            | 16.832           | 0.327            |
| 413.16         | 8.672             | 0.389                       | 453.16            | 18.269           | 0.330            |
| 418.16         | 9.519             | 0.395                       | 458.16            | 19.837           | 0.333            |
| 423.16         | 10.430            | 0.392                       | 463.16            | 21.445           | 0.338            |
| 428.16         | 11.443            | 0.394                       | 468.16            | 23.217           | 0.343            |
| 433.16         | 12.529            | 0.395                       | 473.86*           | 25.279*          | 0 348*           |
| 438.16         | 13.665            | 0.396                       | Perfluoromethyley | clohexane-2,2-Di | imethylbutane    |
| 443.16         | 14.871            | 0.398                       | 398.16            | 7.652            | 0.220            |
| 448.16         | 16.163            | 0 <b>.399</b>               | 403.16            | 8,452            | 0.227            |
| 453.16         | 17.547            | 0.401                       | 408.16            | 9.290            | 0.230            |
| 458.16         | 19.032            | 0.403                       | 413.16            | 10.175           | 0.234            |
| 463.16         | 20.647            | 0.404                       | 418.16            | 11.112           | 0.239            |
| 468.16         | 22.374            | 0.405                       | 423.16            | 12.142           | 0.243            |
| 474.36*        | 24.201*           | 0.407*                      | 428.16            | 13.263           | 0.248            |
| Derfluoromethy | loveloberone_2-M  | athulmantana                | 433.16            | 14.476           | 0.252            |
| 209.16         | 6 700             |                             | 438.16            | 15.738           | 0.257            |
| 402.16         | 7 410             | 0.355                       | 443.16            | 17.076           | 0.262            |
| 405.10         | /.419             | 0.357                       | 448.16            | 18 510           | 0.266            |
| 400.10         | 0.100             | 0.339                       | 453.16            | 20.023           | 0 271            |
| 410.10         | 9.014             | 0.362                       | 458 16            | 21 660           | 0.274            |
| 418,10         | 9,904             | 0.304                       | 462 16            | 21.000           | 0.275            |
| 423.10         | 10.865            | 0.367                       | TUJ.10            | 23.733           | 0.273            |
| 428.16         | 11.911            | 0.372                       | 407.20*           | 20.0637          | 0.2/9*           |

<sup>a</sup> The asterisks denote critical azeotropes.

Table VII. Azeotropic A and B Constants for a Least-Squares Analysis of Eq 1

|                | azeotrop  |           |                      |
|----------------|-----------|-----------|----------------------|
| system         | A         | В         | std dev <sup>a</sup> |
| PFMCH-n-hexane | 4.457 560 | -1466.323 | 0.008 707            |
| PFMCH-2-MP     | 4.445 572 | -1442.199 | 0.003 733            |
| PFMCH-3-MP     | 4.438 409 | -1446.563 | 0.003 889            |
| PFMCH-2.2-DMB  | 4.365 985 | -1387.717 | 0.003 920            |
| PFMCH-2,3-DMB  | 4.419434  | 1429.826  | 0.003 728            |

<sup>a</sup> Standard deviation is the square root of the sum of the squares of of the residuals, divided by the number of data points minus two.

Table VIII. Azeotropic a and b Constants for a Least-Squares Analysis of Eq 2

| azeotropic constant |           |           |          |  |  |
|---------------------|-----------|-----------|----------|--|--|
| system              | a         | Ь         | std dev  |  |  |
| PFMCH-n-hexane      | 4.724130  | 10.044 05 | 0.023 45 |  |  |
| PFMCH-2-MP          | 5.733198  | 10.836 50 | 0.015 89 |  |  |
| PFMCH-3-MP          | 10.404 90 | 23.100 01 | 0.031 01 |  |  |
| PFMCH-2.2-DMB       | 4.143 642 | 4.980 282 | 0.014 34 |  |  |
| PFMCH-2,3-DMB       | 4.782693  | 7.330 248 | 0.01844  |  |  |

Ρ pressure

- R gas constant
- Т thermodynamic temperature

- V volume
- mole fraction x
- density ρ
- ξ binary interaction coefficient

#### Subscripts

1, 2 component 1, 2

- critical value C
- pseudocritical value for mixture cm
- component i, j i, j

#### Superscripts

Α azeotropic value

- G gas
- L liquid

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